## Vertical Curve

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## Profiles:

## Curve a: Crest Vertical Curve (concave downward) <br> Curve b: Sag Vertical Curve (concave upward)



Figure 25-1 Grade line and ground profile of a proposed highway section.

Tangents: Constant Grade (Slope)

## Equal-Tangent Vertical Parabolic Curve:



Figure 25-3 Vertical parabolic curve relationships.

## Terms:

BVC: Beginning of Vertical Curve
V: Vertex
EVC: End of Vertical Curve
aka PVC
aka PVI
aka PVT
$\mathrm{g}_{1}$ : percent grade of back tangent
$\mathrm{g}_{2}$ : percent grade of forward tangent
L: curve length (horizontal distance) in feet or stations
$x$ : horizontal distance from any point on the curve to the BVC
$r$ r: rate of change of grade

## Equations:

$r=\left(g_{2}-g_{1}\right) / L$
where:

$$
\begin{aligned}
& g_{2} \& g_{1} \text { - in percent }(\%) \\
& L-\text { in stations }
\end{aligned}
$$

and
$Y=Y_{B V C}+g_{1} x+(r / 2) x^{2}$
where:
$Y_{B V C}$ - elevation of the BVC in feet

## Example: Equal-Tangent Vertical Curve

Given the information show below, compute and tabulate the curve for stakeout at full 100' stations.



Solution:
(continued)
$r / 2=-0.45 \%$ per station
Elev $_{\mathrm{x}}=$ Elev $_{\text {BVC }}+\mathrm{g}_{1} \mathrm{x}+(\mathrm{r} / 2) \mathrm{x}^{2}$
Elev $_{44+00}=844.48+3.00(0.30)-0.45(0.30)^{2}=845.34{ }^{\prime}$
$\mathrm{Elev}_{45+00}=844.48+3.00(1.30)-0.45(1.30)^{2}=847.62{ }^{\prime}$
$\mathrm{Elev}_{46+00}=844.48+3.00(2.30)-0.45(2.30)^{2}=849.00^{\prime}$ etc.

Elev $_{49+00}=844.48+3.00(5.30)-0.45(5.30)^{2}=847.74^{\prime}$
Elev $_{49+70}=844.48+3.00(6.00)-0.45(6.00)^{2}=846.28$ ' $($ CHECKS $)$

Solution:
(continued)

| Station | $x$ <br> (stations) | $g_{1} x$ | $r / 2 x^{2}$ | Curve <br> Elevation |
| :--- | ---: | ---: | ---: | ---: |
| $43+70$ BVC | 0.0 | 0.00 | 0.00 | 844.48 |
| $44+00$ | 0.3 | .90 | -0.04 | 845.34 |
| $45+00$ | 1.3 | 3.90 | -0.76 | 847.62 |
| $46+00$ | 2.3 | 6.90 | -2.38 | 849.00 |
| $47+00$ | 3.3 | 9.90 | -4.90 | 849.48 |
| $48+00$ | 4.3 | 12.90 | -8.32 | 849.06 |
| $49+00$ | 5.3 | 15.90 | -2.64 | 847.74 |
| $49+70$ EVC | 6.0 | 18.00 | -6.20 | $\underline{846.28}$ |

## High and Low Points on Vertical Curves

Sag Curves:
Low Point defines location of catch basin for drainage.
Crest Curves:
High Point defines limits of drainage area for roadways.
Also used to determine or set elevations based on minimum clearance requirements.

## Equation for High or Low Point on a Vertical Curve:

$y=y_{B V C}+g_{1} x+(r / 2) x^{2}$
Set $d y / d x=0$ and solve for $x$ to locate turning point
$0=0+g_{1}+r x$
Substitute $\left(g_{2}-g_{1}\right) / L$ for $r$
$-g_{1}=x\left(g_{2}-g_{1}\right) / L$
$-g_{1} L=x\left(g_{2}-g_{1}\right)$
$x=\left(-g_{1} L\right) /\left(g_{2}-g_{1}\right)$
or
$x=\left(g_{1} L\right) /\left(g_{1}-g_{2}\right)=g_{1} / r \quad x$ - distance from BVC to HP or LP

## Example: High Point on a Crest Vertical Curve

From previous example:
$g_{1}=+3 \%, g_{2}=-2.4 \%, L=600^{\prime}=6$ full stations, $r / 2=-0.45$,
Elev $_{\text {BVC }}=844.48^{\prime}$
$x=\left(g_{1} L\right) /\left(g_{1}-g_{2}\right)$
$x=(3)(6) /(3+2.4)=3.3333$ stations or 333.33'
HP STA $=$ BVC STA $+x$
HP STA $=4370+333.33=$ HP STA $47+03.33$
$E L E V_{\text {HP }}=844.48+3.00(3.3333)-0.45(3.3333)^{2}=849.48{ }^{\prime}$
Check table to see if the computed elevation is reasonable!

## Unequal-Tangent Parabolic Curve



## Solution:



## Solution (continued):



## Solution (continued):



## Computation of values for $\mathrm{g}_{1} \mathrm{x}$ and $\mathrm{g}_{2} \mathrm{x}$

|  | STATION | $\underline{\mathbf{x}}$ | $\mathrm{g}_{1} \mathrm{x}$ | (r/2) $\mathrm{x}^{2}$ | Curve Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BVC | $83+00$ | 0 | 0 | 0 | 751.24' |
|  | $84+00$ | 1 | -2.00 |  |  |
|  | $85+00$ | 2 |  |  |  |
|  | $86+00$ | 3 |  |  |  |
| CVC | $87+00$ | 4 |  |  | 747.56' |
|  | $88+00$ | 1 | 0.16 |  |  |
|  | $89+00$ | 2 |  |  |  |
|  | $90+00$ | 3 |  |  |  |
|  | $91+00$ | 4 |  |  |  |
|  | $92+00$ | 5 |  |  |  |
| EVC | $93+00$ | 6 |  |  |  |
|  |  |  |  |  |  |
|  |  |  | $\mathrm{g}_{1} \mathrm{x}=$ | -2 (1) = | -2.00 |
|  |  |  | $\mathrm{g}_{2} \mathrm{x}=$ | $.16(1)=$ | 0.16 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## Computation of values for $\left(r_{1} / 2\right) x^{2}$ and $\left(r_{2} / 2\right) x^{2}$

|  | STATION | $\underline{\text { x }}$ | $\underline{\mathbf{G}_{1} \mathbf{x}}$ | $(r / 2) x^{2}$ | Curve Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BVC | $83+00$ | 0 | 0 | 0 | 751.24' |
|  | $84+00$ | 1 | -2.00 | 0.27 |  |
|  | $85+00$ | 2 | -4.00 |  |  |
|  | $86+00$ | 3 | -6.00 |  |  |
| CVC | $87+00$ | 4 | -8.00 |  | 747.56' |
|  | $88+00$ | 1 | 0.16 | 0.12 |  |
|  | $89+00$ | 2 | 0.32 |  |  |
|  | $90+00$ | 3 | 0.48 |  |  |
|  | $91+00$ | 4 | 0.64 |  |  |
|  | $92+00$ | 5 | 0.80 |  |  |
| EVC | $93+00$ | 6 | 0.96 |  |  |
|  |  |  |  |  |  |
|  |  |  |  | $\left(r_{1} / 2\right) \mathrm{x}^{2}$ | $=(0.27)(1)^{2}=0.27$ |
|  |  |  |  | $\left(r_{2} / 2\right) x^{2}$ | $=(0.12)(1)^{2}=0.12$ |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## Elevation Computations for both Vertical Curves

|  | STATION | $\underline{\text { x }}$ | $\underline{g_{1} x}$ | $(\mathrm{r} / 2) \mathrm{x}^{2}$ | Curve Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BVC | $83+00$ | 0 | 0 | 0 | 751.24' |
|  | $84+00$ | 1 | -2.00 | 0.27 |  |
|  | $85+00$ | 2 | -4.00 | 1.08 |  |
|  | $86+00$ | 3 | -6.00 | 2.43 |  |
| CVC | $87+00$ | 4 | -8.00 | 4.32 | 747.56' |
|  | $88+00$ | 1 | 0.16 | 0.12 |  |
|  | $89+00$ | 2 | 0.32 | 0.48 |  |
|  | $90+00$ | 3 | 0.48 | 1.08 |  |
|  | $91+00$ | 4 | 0.64 | 1.92 |  |
|  | $92+00$ | 5 | 0.80 | 3.00 |  |
| EVC | $93+00$ | 6 | 0.96 | 4.32 |  |
| $Y_{1}=751.24-2.00+0.27=749.51^{\prime}$ |  |  |  |  |  |
| $Y_{2}=747.56+0.16+0.12=747.84{ }^{\prime}$ |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## Computed Elevations for Stakeout at Full Stations

|  | STATION | $\mathbf{x}$ | $\mathbf{g}_{1} \mathbf{x}$ | $\left(\mathbf{r} / \mathbf{2 )} \mathbf{x}^{\mathbf{2}}\right.$ | Curve Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BVC | $83+00$ | 0 | 0 | 0 | $751.24^{\prime}$ |
|  | $84+00$ | 1 | -2.00 | 0.27 | $749.51^{\prime}$ |
|  | $85+00$ | 2 | -4.00 | 1.08 | $748.32^{\prime}$ |
| CVC | $86+00$ | 3 | -6.00 | 2.43 | $747.67^{\prime}$ |
|  | $87+00$ | 4 | -8.00 | 4.32 | $747.56^{\prime}$ |
|  | $88+00$ | 1 | 0.16 | 0.12 | $747.84^{\prime}$ |
|  | $89+00$ | 2 | 0.32 | 0.48 | $748.36^{\prime}$ |
|  | $90+00$ | 3 | 0.48 | 1.08 | $749.12^{\prime}$ |
|  | $91+00$ | 4 | 0.64 | 1.92 | 750.12 |
| EVC | $92+00$ | 5 | 0.80 | 3.00 | $751.36^{\prime}$ |
|  | $93+00$ | 6 | 0.96 | 4.32 | $752.84^{\prime}$ |
|  |  |  |  |  |  |

## Designing a Curve to Pass Through a Fixed Point



Figure 25-8 Designing a parabolic curve to pass through a fixed point.

## Solution:



Figure 25-8 Designing a parabolic curve to pass through a fixed point.

## Solution (continued):

$1271.20=\left[1261.50+4.00\left(\frac{L}{2}\right)\right]+\left[-4.00\left(\frac{L}{2}+1.5\right)\right]+\left[\frac{3.80+4.00}{2 L}\left(\frac{L}{2}+1.5\right)^{2}\right]$
$0.975 L^{2}-9.85 L+8.775=0$
$x=\frac{-b \pm \sqrt{b^{2}-4 a c}}{2 a}$
$a=0.975$
$b=-9.85$
$c=8.775$
$L=9.1152$ stations $=911.52^{\prime}$


Figure 25-8 Designing a parabolic curve to pass through a fixed point.

## Sight Distance

- Defined as "the distance required, for a given design speed to safely stop a vehicle thus avoiding a collision with an unexpected stationary object in the roadway ahead" by AASHTO (American Association of State Highway and Transportation Officials)
- Types
- Stopping Sight Distance
- Passing Sight Distance
- Decision Sight Distance
- Horizontal Sight Distance


## Sight Distance Equations

$$
\begin{aligned}
& \text { For Sag Curves } \\
& S \leq L \\
& L=\frac{S^{2}\left(g_{2}-g_{1}\right)}{4+3.5 S} \\
& S \geq L \\
& L=2 S-\frac{4+3.5 S}{g_{1}-g_{2}}
\end{aligned}
$$

